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Simulation of Pedestrian Protection in LS-DYNA LS-DYNA 行人保护仿真介绍

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Pedestrian Protection Overview

Scenario: vehicle frontend hits crossing pedestrian

Factors determine injuries

- Vehicle speed
- Pedestrian height
- Frontend shape
- Hood length



For regulatory and NCAP testing:

impactors representing different human body parts hit vehicle frontend

Model capacities required

- Windshield
- Hood
- Frontend
- Pedestrian





How to...

accurately model the key components like windshield?

design a better hood for less severe injury?

better represent a pedestrian?





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A Model for Laminated Glass Discretization

- Laminated glass consists of at least 3 layers
 - 2 glass panes: shell elements with MAT_GLASS (MAT_280)
 - PVB interlayer: transverse shear deformation important
 → solid elements
- Contact between layers: shared nodes
- Offset the glass layers with NLOC parameter (SECTION_SHELL)



- Glass fragments are bonded
 - Difficult mechanical behavior







Introduction to MAT_GLASS (280) Theoretical Background

- Linear elastic until failure
- Stress based failure criteria: Rankine, Mohr-Coulomb, Drucker-Prager
- Compressive failure
 - Material is 'crumbled'
- Tensile failure
 - Single Cracks
 - Crack direction perpendicular to the 1st principal stress
 - 2nd crack can occur orthogonal to the 1st crack
 - Cracks can open and close independently
- Elements will not be automatically deleted when failed
- EPSCR (MAT_GLASS) or MAT_ADD_EROSION can help deleting distorted elements







Strength Reduction

- Stress concentration in tip of crack
 - Cannot be resolved by coarse FE-mesh
 - To consider this effect in MAT_280 the tensile strength can be reduced after the first crack

IMOD

BC

Combination of variables determines the way the strength reduction works









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 $FTSCL \times FT$

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New option for *MAT_280



- ENGCRT/RADCRT: failure model described by Pytell/Liebertz (2011)
 - Initially deactivates failure/cracks
 - 1st element with $\sigma_{\rm max}$ >"FT"×"FTSCL" defines center of impact
 - Internal energy of part within radius RADCRT is monitored
 - When internal energy reaches ENGCRT, failure is activated
- NEW: critical energy depends on edge distance
 - ENGCRT<0 refers to *DEFINE_FUNCTION, e.g.,



```
*DEFINE_FUNCTION
			100
float func(float distx) {
		float engx;
		engx=min(0.03*distx,7.3);
$ printf("DISTANCE=%.7e, ENERGY=%.7e\n",distx,engx);
		return engx;
}
```



Stochastic Variation

- Stochastically distributed tensile strength due to microcracks
- *MAT_280_STOCHASTIC +
 *DEFINE_STOCHASTIC_VARIATION
 → stochastically distributed factor for tensile strength
- Kind of distribution is given by VAR_S
 - 1: Uniform random distribution
 - 2: Normal distribution
 - 3: User defined probability distribution
 - 4: User defined cumulative distribution
- History variable #13 shows factor



Glass strength prediction model

Available as *MAT_GLASS_SPM

- Monte-Carlo based fracture initiation predictor
- combines the theories of linear elastic fracture mechanics (LEFM) and sub-critical crack growth (SCG)
- generates a representative sample of virtual glass plates which are monitored during the simulation
- GSPM predicts tensile strength, initiation location, and initiation time for the 1st crack, then *MAT_280 takes over for crack propagation
- Model details and calibration procedure for new parameters described in Rudshaug et al. (2023)







Glass strength prediction model

- Capabilities of the new method
 - Can describe the probabilistic fracture behavior of glass and SCG
 - Predicts the strength of glass plates of various geometries exposed to many different load cases
 - User can select a representative case of a glass plate fracture strength simply by altering the failure percentile parameter
 - Example: windshield impact





Position-Based Tensile Strength

Laminated glass

- tensile strength varies over thickness
- Options to consider effect in LS-DYNA
 - INTEGRATION_SHELL
 - PART_COMPOSITE
- INTEGRATION_SHELL is more flexible
 - Integration rule can be defined
 - For each ply, an individual stochastic variation can be defined



*PART						
Glass out	er pane					
\$ PI	D SECID	MID	EOSID	HGID	GRAV	ADPOPT
10	0 (100) 100	0	0	0	0
*SECTION_	SHELL					
\$ SECI	DELFORM	SHRF	NIP	PROPT	QR/IRID	ICOMP
10	2	0.833	3	1.0	-100	0
*INTEGRAT	ION_SHELL					
\$ Gauss-L	obatto inte	gration 3 I	Ps			
\$ IRI	D NIP	ESOP	FAILOPT			
10	3					
Ş	S WF	PID				
-1.0000	0.3333333	101				
0.0000	0 1.3333333	101				
1.0000	0.3333333	102				
*PART						
DUMMY PAR	r - Glass o	iter pane –	air side	- position	1	
\$ PI	D SECID	MID	EOSID	HGID	GRAV	ADPOPT
10:	2 100	102	0	0	0	0
*MAT_GLAS	S					
\$ MI	D RO	E	PR			IMOD
10:	2 2.5E-6	70	0.23			
\$ FMO	D FT	FC	AT	BT	AC	BC
	&ft1					



Position-Based Tensile Strength

- Laminated glass
 - tensile strength varies over thickness
- Options to consider effect in LS-DYNA
 - INTEGRATION_SHELL
 - PART_COMPOSITE
- INTEGRATION_SHELL is more flexible
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*PART		SITE					
Glass	outer	pane					
\$	PID	ELFORM	SHRF	NLOC	MAREA	HGID	ADPOPT
	100	2	0.833			4	
\$	MID1	THICK1	B1	TMID1	MID2	THICK2	B2
	100	0.05					
	100	0.5					
	100	0.5					
	100	0.5					
	100	0.5					
	200	0.05					
*MAT	GLASS !	FITLE					
PVB s	ide 🗕						
\$	MID	RO	Е	PR			IMOD
	100	2.5E-6	70	0.23			
\$	FMOD	FT	FC	AT	BT	AC	BC
	& 1	Et2					
*MAT	GLASS 1	FITLE					
air s	side						
\$	MID	RO	E	PR			IMOD
	200	2.5E-6	70	0.23			
\$	FMOD	FT	FC	AT	BT	AC	BC
	& 1	Et1					



Crack visualization Option I

Head impact on windshield

- Cracks can be visualized as a vector plot using history variables #15, #16, and #17
 - Crack direction is shown
 - So far only shows 1st crack
 - Available since R15





		•
Vector Plot X	FriComp	RefGeo
Hist, var. cosine 🗸	Ø	ູ່
	FriRang	Curve
	Hist	$\langle \rangle$
	History	Surf
H.var X H.var Y H.var Z	xy	
15 16 17	XYPlot	Solid
Int. Pt. 1	Ascii	ø
Vector Range	ASCII	GeoTol
Min: 0	Bin Out	(Pro-
Max: 0	Binout	*## Mesh
	>>	6
Dynamic Ostatic	Follow	Model
O User O Show	\leq	2-2-9
SF: 2.0 × 2	Trace	5-5-1 EleTol
		M
Hidden line vector off	State	Post
Keep vector display	-	
Apply settings in Range	Particle	MS
Display highlighted node vel.	101	MS
Force resultant	ChaiMd	4
Prin. int.pt.		Favor1
None	Output	
Whole OPart	1v	
⊖ Area ⊖ El/Node	Vector	
Apply Clear	1	
	FLD	
Save Done:	315	
	BotDC	
	1	
	Cracks	

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Crack visualization

Option II

- Head impact on windshield
- Cracks can be visualized by history variable #1 of MAT_GLASS
 - -1: compressive failure
 - 0: no failure
 - 1: one crack
 - 2: two cracks









How to...

accurately model the key components like windshield?

design a better hood for less severe injury?

better represent a pedestrian?



Topology Optimization using LS-TaSC

- Topology and shape optimization of non-linear problems
- Multiple load cases and disciplines
- Global constraint handling
 - Energy absorption, maximum reaction forces, ...
 - \rightarrow Multi-point optimization and metamodels
- Redistribution of material within a given domain
- Design variables
 - Relative density of each element
- Result
 - New material distribution
 - New shape of structure





LS-TaSC Algorithm



• Objective: Stiffest structure, satisfy constraints and minimize mass • Constraints: rear beam, bending and torsion displacements **Outer skin (shell)** Optimum **Design part (solid)** Initial Design has very low mass fraction of 0.01. Rear beam Torsion **Design Contribution Plot** Bending Model by courtesy of Jaguar Land Rover (Rear beam, torsion, bending)

Hood Design Optimization using LS-TaSC



Integration





Active hood system

• Active hoods to provide more deformation space between the hood and the engine compartment package



- Sensing system to identify a pedestrian impact (fiberoptics, pressure tube)
- Active system (actuator at hinge) to deploy the hood
- Special requirements to prove that hood is fully deployed prior to the head impact



Pressure tube sensor

- Pressure tubes along the bumper foam
- Sensing locations at the ends of the tube



- Impact will compress tube and create pressure wave traveling along the tube
- Tube modeling including physical properties defined by *DEFINE_PRESSURE_TUBE



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Reference: "Recent Developments in *DEFINE PRESSURE TUBE for Simulating Pressure Tube Sensors in Pedestrian Crash" by Jesper Karlsson

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Introducing HANS

- Hans is a high-fidelity LS-DYNA human body model
- Commercial model licensed separately
- Hans represents an average male person AM50
 - Body Specs: ~77kg, 176cm, BMI 24.9, Age 30-40
 - Model size
 - Number of nodes: ~1.6Mio
 - Number of elements: ~2Mio
 - Number of parts: 1,978
 - Macro Fiber Parts (keep adding): 138
 - Contacts
 - 1 single surface contact
 - 5 tied contacts to attach soft tissue
 - Recommended time step: 0.5µsec





Modeling Fundamentals

- Passive model targeted for any kind of explicit impact simulation
- Focus on the musculoskeletal system at first
- Modeling the physics:
 - Model the human body with a high level of detail



- Avoiding abstraction and substitute approaches
 - Geometry and materials are modeled as is
 - \rightarrow Less tweaking needed to correlate to test data
 - Better confidence in load cases that are not covered by test
- Following the modeling approaches of the successful DYNAmore Dummy models





Motivation

Product development

- So far, many industries rely on physical and virtual dummies for product development
- Human Body models can overcome some downsides of dummies, as they are
 - a more accurate approximation of a human
 - are **non-directional**
- Increasingly sophisticated safety systems and new application areas require higher fidelity models
 - "Made for humans not for dummies"

Product Certification

- There are initiatives in serveral industries to establish virtual product certification using HBMs
 - EuroNCAP, IIHS, C-NCAP, ... are actively working on such protocols
 - DYNAmore/ANSYS is involved in the EuroNCAP activities
 - Virtual Tests require qualified human body models



- ...



Vulnerable Road Users (VRUs) – EuroNCAP TB024



- Qualification model included in the delivery package
- In total 9 (3 generic vehicles x 3 impact speeds) are carried out for qualification





How to... in summary

accurately model the key components like windshield?

Laminated glass model with MAT_GLASS + added features

design a better hood for less severe injury?

Use optimization tools such as LS-TaSC and active hood

better represent a pedestrian?

HANS! For virtual certification







SimAl Objective



Several Designs





SimAl – General Idea

SimAI possesses several unique features:

- (i) it is robust to varying mesh sampling, allowing for adaptability to different geometries,
- (ii) it effectively captures multi-scale phenomena, resulting in stateof-the-art scores for both volume and surface evaluations,
- (iii) as a continuous surrogate model, it can be used to accelerate the evaluation of different geometries during the design process, leading to significant speed-up.



- Encode the distance function and the normal components into latent codes
- Use the latent codes to infer predicted output codes
- Decode the output codes with modulated INRs to get the physical fields
- SimAI uses a proprietary Architecture slightly different from the one shown above



- Iotal data of 106 simulations
 - Training set : 86 simulation Data points
 - Testing Data set : 20 Simulation Data points

Pedestrian Head Impact

- Challenge
 - For Pedestrian Head Impact, a grid of around 200 points on the hood are evaluated for predicted HIC value.
 - Needs to be repeated for every design change
- SimAl + LS-DYNA
 - Instead of running all 200 points, Run the simulation on 100 points. Predict HIC value for remaining points using SimAI
 - Total data of 106 simulations- 86 training set & 20 testing set



Pedestrian Head Impact : SimAl Model

- Total data of 106 simulations
 - Training set : 86 simulation Data points
 - Testing Data set : 20 Simulation Data points
 - Typical Data Point :
 - json file with input parameters
 - E.g. this case , We have considered Time
 - .vtp file : which contained displacement field and HIC value
 - .vtu file : For cast component, it has displacement field

		21		
🧾 boundary_condition.json	17-06-2024 16:47	JSON File	1 KB	
📶 surface.vtp	17-06-2024 16:47	VTP File	47,856 KB	
📶 volume.vtu	17-06-2024 16:47	VTU File	5,272 KB	



{"Time": 29.99936866760254}

json file





Model Configuration and Evaluation Report

Model configuration

3.5.1 Test geometry 118

Reference sample

ML_Pdst_v4_C.5.7_28 👤

- Boundary Condition: boundary_condition.json
- Surface file: surface.vtp
- Volume file: volume.vtu

Input/Output = <u>Select variables</u>

Model Inputs Model Outputs Geometry Volume • HIC · Extracted from the surface • U[X] Surface • U[Y] No input • U[Z] **Boundary Conditions** Surface Time • HIC U[X] • U[Y]

✓ Your variables are set

Your volume is set

Your reference sample is valid

Global Coefficients

- HIC_global, in this case 6.454e+2 • U-Normed, in this case 1.962e+2
- Ux_max, in this case 1.679e+2
- Uy_max, in this case 3.659e+1 Uz_max, in this case 4.577e+1

Create coefficient





(a) SimAl prediction (Solver scale)





(b) Solver target (Solver scale)

Figure 20: Geometry mesh of U[Z]

2.2.1 HIC_global



Figure 1: HIC global trend comparison plot

(c) Difference (Zoomed scale)

Domain of Analysis

Define domain of analysis

x position relative to design edge	Volxmin = xmin - 247.627	Length = 2971.527
y position relative to design edge	Volymin = ymin - 220.333	Width = 2643.992
z position relative to design edge	Volzmin = zmin - 142.907	Height = 1714.888

U[Z]

Build duration

O Debug 🐼 4 Data, 30min build

Production



Precise







Pedestrian Head Impact : SIMAI Prediction



Fields	SimAl	Solver	% Error
Maximum Displacement	178.3	179.0	0.4
HIC Value	532.9	518.3	2.8



Fields	SimAl	Solver	% Error
Maximum Displacement	229.1	230.7	0.7
HIC Value	532.9	518.3	2.8



AI ML | Pedestrian Head Impact

- Solver Time : 1hr on 96 CPUs
- SimAl Prediction Time : < 1min



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Fields	SimAl	Solver	% Error
Maximum Displacement	169	174	2.87
HIC Value	522	507	2.95

20 locations previously unseen by the model



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HIC value Prediction

Average Predicting Error is less than 2%

Improved Delivery Positions

- Occupant delivery position modified based on *Rieger et al (2023)*
- Spine angle measurements from volunteer scans in car seats



- Given the same H-Point location, the posture of Hans is close to the postures of WorldSID50M and THOR-50M
- Hans delivery position is aligned with Dummy model positions



 The Pedestrian Position completely fulfils the EuroNCAP TB024 requirements







Summary

- Hans V1.2 comes with a lot of improvements for automotive customers in terms of usability and performance.
- The new release prepares the model for the upcoming/existing EuroNCAP requirements
- **R12.2** is the model development version and required to use Hans
- Included to the delivery package:
 - model in standing and sitting postures One Model
 - Human Body Model in three unit-systems, including parameterized renumbering
 - Accessoires like shoes, ...
 - Treefile for positioning of the model in the commonly used pre-processing tools
 - Documentation/Correlation report
 - 1st class global expert support







Required simulation capabilities

- Material properties
 - Plastic materials (headlamps, front fascia, ...)
 - Including fracture
 - Windshield glass
 - Fracture and crack propagation
 - Displacement (potential secondary impact with instrument panel)
- Package parts
 - Powertrains
 - Electronic components
 - Hinges

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- Cables and cable bundles
- Instrument panels including all parts in potential impact area

Modeling of package components

Simplified electric cable modeling with *DEFINE_CABLE

- Simple creation and analysis of electric cables for modeling wire failure in vehicle crash
 - Automatic creation of cables from beam elements
 - Final cables can be a mix of solids/shells/beams
 - Links cross-section data to each original beam element
- Data available in binout (*DATABASE_CABLE: cableout)
 - Compression (contact) force
 - Cross-section area
- Data summary available in ASCII-file
 - Time and location for maximum compression force and minimum cross-section area for each cable and for whole model



Data summary

PART-WISE DA	TA:					
Beam part= maxstress= minarea = maxforce =	83990001, sampling freq 0.4953E-01, time= 0.5891E+02, time= 0.5590E+01, time=	uency= 0.5000E+01, 0.5000E+01, 0.4998E+01,	1 cycles element= element= element=	46 48 46		
Beam part= maxstress= minarea = maxforce =	83990002, sampling freq 0.7170E-01, time= 0.8419E+02, time= 0.9542E+01, time=	uency= 0.4991E+01, 0.4997E+01, 0.4997E+01,	10 cycles element= element= element=	6020579 6020579 6020579		
Beam part= maxstress= minarea = maxforce =	83990005, sampling freq 0.3333E-03, time= 0.3247E+03, time= 0.0000E+00, time=	uency= 0.4854E+01, 0.2972E+01, 0.0000E+00,	1 cycles element= element= element=	6020613 6020613 0		
Beam part= maxstress= minarea = maxforce =	83990006, sampling freq 0.5296E-03, time= 0.8662E+02, time= 0.0000E+00, time=	uency= 0.2155E+01, 0.2664E+01, 0.0000E+00,	1 cycles element= element= element=	6020623 6020623 0		
DATA FOR ALL	PARTS:					
maxstress= minarea = maxforce =	0.7170E-01, time= 0.5891E+02, time= 0.9542E+01, time=	0.4991E+01, 0.5000E+01, 0.4997E+01,	element= element= element=	6020579, 48, 6020579,	part= part= part=	83990002 83990001 83990002

